

Brownian motion with inertia

(1)

$$\boxed{m \frac{du}{dt} = -\gamma u + \tilde{A}'(t)}, \quad \frac{du}{dt} = -5u + \tilde{A}(t) \Rightarrow \underbrace{e^{5t} \left(\frac{du}{dt} + 5u \right)}_{\frac{d}{dt} (u e^{5t})} = A e^{5t}$$

$$u(0) = u_0$$

$$\text{so, } u e^{5t} - u_0 = \int_0^t dt' e^{5t'} \tilde{A}(t')$$

$$\text{or } \boxed{U = u(t) - u_0 e^{-5t} = e^{-5t} \int_0^t dt' e^{5t'} \tilde{A}(t')} \Rightarrow \langle U \rangle = e^{-5t} \int_0^t dt' e^{5t'} \langle \tilde{A}(t') \rangle = 0$$

higher moments:

$$\langle U^2 \rangle = \langle u^2 \rangle - 2 \langle u \rangle u_0 e^{-5t} + u_0^2 e^{-25t} = \langle u^2 \rangle - u_0^2 e^{-25t}$$

$$= e^{-25t} \int_0^t dt' \int_0^t dt'' e^{5(t'+t'')} \underbrace{\langle \tilde{A}(t') \cdot \tilde{A}(t'') \rangle}_{\phi(t'-t'') \text{ (hypothesis)}}$$

$$\text{let } t'+t''=x \quad t' = \frac{x+y}{2} \\ t'-t''=y \quad t'' = \frac{x-y}{2}$$

$$\text{Jacobian } \begin{pmatrix} \partial x / \partial t' & \partial x / \partial t'' \\ \partial y / \partial t' & \partial y / \partial t'' \end{pmatrix} = \begin{vmatrix} 1 & 1 \\ 1 & -1 \end{vmatrix} = 2$$

$$= \frac{1}{2} e^{-25t} \int_0^{2t} e^{5x} dx \underbrace{\int_{-\infty}^{\infty} \phi(y) dy}_{\substack{\text{extends limits by} \\ \text{virtue of short-range} \\ \text{feature of } \phi}} \equiv \tau$$

$$\Rightarrow \langle U^2 \rangle = \frac{1}{2} e^{-25t} \tau \cdot \frac{1}{5} (e^{25t} - 1) = \boxed{\frac{\tau}{25} (1 - e^{-25t})}$$

$$\text{as } t \rightarrow \infty, \langle U^2 \rangle \text{ satisfies } \frac{1}{2} m \langle U^2 \rangle = \frac{3}{2} k_B T \text{ (equipartition)}$$

$$\text{or } \langle U^2 \rangle = 3k_B T / m$$

$$\text{so, } \frac{\tau}{25} = \frac{3k_B T}{m}$$

$$\boxed{\langle U^2 \rangle = \frac{3k_B T}{m} (1 - e^{-25t})}$$

To evaluate higher moments, we note that since $\langle \tilde{A} \rangle = 0$, all odd moments = 0. For the even moments we'll have to evaluate expressions of the form

↓

$$e^{-2n\gamma t} \int dt_1 \dots \int dt_{2n} e^{\gamma(t_1 + \dots + t_{2n})} \langle \underline{A}(t_1) \underline{A}(t_2) \dots \underline{A}(t_{2n}) \rangle$$

doing this by pairs will give the same contribution per pair as $\langle U^2 \rangle$, yielding $\langle U^2 \rangle^n$, with a prefactor given by the number of distinct pairs we can choose from $2n$ labels $t_1, \dots, t_{2n}$. With $2n$ labels there are n pairs:

$$\text{the \# of ways is } \frac{(2n)!}{n! 2^n} = \frac{2n(2n-1)(2n-2)(2n-3) \dots}{n(n-1)(n-2) \dots 2^n} = (2n-1)!!$$

$\nwarrow$ permuting pairs $\swarrow$ switching within pairs

$$\therefore \langle U^{2n} \rangle = (2n-1)!! \langle U^2 \rangle^n = (2n-1)(2n-3) \dots 5 \cdot 3 \cdot 1 \cdot \langle U^2 \rangle^n$$

For a Gaussian distribution this is exactly the case

$$\begin{aligned} \langle U^2 \rangle &= 1! \langle U^2 \rangle \\ \langle U^4 \rangle &= 3 \langle U^2 \rangle^2 \\ \langle U^6 \rangle &= 15 \langle U^2 \rangle^3 \end{aligned}$$

$$\therefore P(u, t; u_0, 0) = \left[\frac{m}{2\pi k_B T (1 - e^{-2\gamma t})} \right]^{3/2} \exp \left\{ -\frac{m}{2k_B T (1 - e^{-2\gamma t})} |\underline{u} - \underline{u}_0 e^{-\gamma t}|^2 \right\}$$

$$\text{since } \underline{u}(t) = \underline{u}_0 e^{-\gamma t} + \int_0^t dt' e^{-\gamma(t-t')} \underline{A}(t') ; \quad \underline{r} - \underline{r}_0 = \int_0^t dt' \underline{u}(t')$$

$$\Rightarrow \underline{r} - \underline{r}_0 = \int_0^t dt' \left[\underline{u}_0 e^{-\gamma t'} + \int_0^{t'} dt'' e^{-\gamma(t'-t'')} \underline{A}(t'') \right]$$

$$\underline{r} - \underline{r}_0 - \frac{1}{\gamma} (1 - e^{-\gamma t}) \underline{u}_0 = \int_0^t dt' \int_0^{t'} dt'' e^{-\gamma(t'-t'')} \underline{A}(t'')$$

integrate by parts:

$$dv = dt' e^{-\gamma t'} \quad u = \int_0^{t'} dt'' e^{\gamma t''} \underline{A}(t'')$$

$$v = -\frac{1}{\gamma} e^{-\gamma t'} \quad du = \gamma e^{\gamma t'} \underline{A}(t') dt'$$

$$-\frac{1}{\gamma} e^{-\gamma t'} \int_0^{t'} dt'' e^{\gamma t''} \underline{A}(t'') \Big|_0^t + \frac{1}{\gamma} \int_0^t dt' e^{-\gamma t'} e^{\gamma t'} \underline{A}(t')$$

$$= -\frac{1}{\gamma} e^{-\gamma t} \int_0^t dt' e^{\gamma t'} \underline{A}(t') + \frac{1}{\gamma} \dots = \frac{1}{\gamma} \int_0^t dt' [1 - e^{-\gamma(t-t')}] \underline{A}(t')$$

change label

$$\Rightarrow \langle \underline{r} - \underline{r}_0 \rangle = \frac{\underline{u}_0 (1 - e^{-\gamma t})}{\gamma}$$

Calculate the variance: $\hat{r} - \hat{r}_0 - \frac{u_0}{\gamma} (1 - e^{-\gamma t}) = \frac{1}{\gamma} \int_0^t dt' [1 - e^{-\gamma(t-t')}] \underline{A}(t')$ Brownian motion w/inertia

(3)

$$|\hat{r} - \hat{r}_0|^2 - 2(\hat{r} - \hat{r}_0) \cdot \frac{u_0}{\gamma} (1 - e^{-\gamma t}) + \frac{u_0^2}{\gamma^2} (1 - e^{-\gamma t})^2$$

$$= \frac{1}{\gamma^2} \int_0^t dt' \int_0^t dt'' [1 - e^{-\gamma(t-t')}] [1 - e^{-\gamma(t-t'')}] \underline{A}(t') \cdot \underline{A}(t'')$$

$$1 - e^{-\gamma t + \gamma t'} - e^{-\gamma t + \gamma t''} + e^{-2\gamma t + \gamma(t'+t'')}$$

$\langle \rangle \Rightarrow$

$$\langle |\hat{r} - \hat{r}_0|^2 \rangle - \frac{u_0^2}{\gamma^2} (1 - e^{-\gamma t})^2 = \frac{1}{\gamma^2} \int_0^t dt' \int_0^t dt'' \underbrace{\langle \underline{A}(t') \cdot \underline{A}(t'') \rangle}_{\frac{1}{2} \int dx x = \frac{1}{2} \tau} \underbrace{- e^{-\gamma t} \int_0^t dt' \int_0^t dt'' e^{\gamma t'} \langle \underline{A} \underline{A} \rangle}_{e^{-\gamma t} \frac{1}{2} \int dx x^2 \int dy y}$$

$$= -\frac{\tau}{\gamma} (1 - e^{-\gamma t})$$

$$- e^{-\gamma t} \int_0^t dt' \int_0^t dt'' e^{\gamma t''} \langle \underline{A} \underline{A} \rangle$$

$$\text{as previous} = -\frac{\tau}{\gamma} (1 - e^{-\gamma t})$$

$$+ e^{-2\gamma t} \int_0^t dt' \int_0^t dt'' e^{\gamma(t'+t'')} \langle \underline{A} \underline{A} \rangle$$

$$\frac{\tau}{2\gamma} (1 - e^{-2\gamma t})$$

$$\text{so, } \langle |\hat{r} - \hat{r}_0|^2 \rangle - \frac{u_0^2}{\gamma^2} (1 - e^{-\gamma t})^2 = \frac{\tau}{\gamma^2} \left[t - \frac{2}{\gamma} (1 - e^{-\gamma t}) + \frac{1}{2\gamma} (1 - e^{-2\gamma t}) \right]$$

$$\tau = \frac{3k_B T}{m} \cdot 2\gamma$$

$$= \frac{3k_B T}{m \gamma^2} \left[2\gamma t - 4(1 - e^{-\gamma t}) + 1 - e^{-2\gamma t} \right]$$

$$= \boxed{\frac{3k_B T}{m \gamma^2} (2\gamma t - 3 + 4e^{-\gamma t} - e^{-2\gamma t})}$$

for small t $2\gamma t - 3 + 4(1 - \gamma t + \frac{1}{2}\gamma^2 t^2 - \frac{1}{6}\gamma^3 t^3 + \dots) - 1 + 2\gamma t - \frac{1}{2}4\gamma^2 t^2 + \frac{1}{6}8\gamma^3 t^3 + \dots$

$$\approx 0(\gamma^3 t^3)$$

$$\text{so } \langle |\hat{r} - \hat{r}_0|^2 \rangle \approx \frac{u_0^2}{\gamma^2} \cdot \gamma^2 t^2 \approx u_0^2 t^2 \quad \text{"ballistic"}$$

↓

for small t the initial conditions are remembered.

for large t ($\zeta t \gg 1$),

$$\langle |\vec{r} - \vec{r}_0|^2 \rangle - \frac{u_0^2}{\zeta^2} \approx \frac{3k_B T}{m\zeta^2} (2\zeta t - 3)$$

$\uparrow$
 dominant term

$$\langle |\vec{r} - \vec{r}_0|^2 \rangle \approx \frac{6k_B T}{m\zeta} t$$

but $m\zeta = \gamma$ (original eqn)

$$\frac{6k_B T}{m\zeta} = \frac{6k_B T}{\gamma} = 6D$$

$$\langle |\vec{r} - \vec{r}_0|^2 \rangle \approx 6Dt$$

diffusion in
three dimensions!

Polymerization

(1)

$$\dot{j} = -D \frac{\partial p}{\partial x} - \frac{F}{5} p \quad \frac{\partial \dot{j}}{\partial t} = -\frac{\partial j}{\partial x}$$

$F=0$, steady state $\frac{\partial^2 p}{\partial x^2} = 0 \Rightarrow p(x) = A + Bx$ with $\int_0^l dx p(x) = 1$ and $p(l) = 0$

$$Al + \frac{1}{2}Bl^2 = 1 \quad A + Bl = 0$$

$$-Bl^2 + \frac{1}{2}Bl^2 = 1 = -\frac{1}{2}Bl^2$$

$$B = -\frac{2}{l^2}; A = \frac{2}{l}$$

$$\dot{j} = -D \frac{\partial p}{\partial x} = -D \cdot B = \frac{2D}{l^2}$$

$$\left[\dot{j} = \frac{2D}{l^2} \Rightarrow \tau_1 = \frac{l^2}{2D} \right] \text{ "velocity" } = l/\tau_1 = 2D/l$$

$F \neq 0$

$$\dot{j} = -D \frac{dp}{dx} + \frac{F}{5} p$$

homogeneous solution is just $-D \frac{dp_h}{dx} = \frac{F}{5} p_h$

$$p_h = A \exp(-Fx/5D) \text{ but } D5 = k_B T \text{ (Stokes-Einstein)}$$

$$= A e^{-\beta Fx}$$

inhomogeneous (particular) sol'n

$$\text{is } \left[p_{in} = -\frac{5\dot{j}}{F} \right] \text{ constant}$$

again, two requirements on the sum $p(x) = A e^{-\beta Fx} - \frac{5\dot{j}}{F}$

$$p(l) = 0 : A e^{-\beta Fl} - \frac{5\dot{j}}{F} = 0$$

$$\int_0^l dx p(x) = 1 = \frac{A}{-\beta F} (e^{-\beta Fl} - 1) - \frac{5\dot{j}l}{F}$$

$$-\frac{5\dot{j}}{F} = -A e^{-\beta Fl}$$

$$\frac{A}{\beta F} (1 - e^{-\beta Fl}) - Al e^{-\beta Fl} = 1 \text{ or } \frac{A}{\beta F} \{ 1 - e^{-\beta Fl} - \beta Fl e^{-\beta Fl} \} = 1$$

$$A = \frac{\beta F}{1 - (1 + \beta Fl) e^{-\beta Fl}} \quad \dot{j} = \frac{FA}{5} e^{-\beta Fl} = \frac{\beta F^2}{5} \frac{e^{-\beta Fl}}{1 - (1 + \beta Fl) e^{-\beta Fl}}$$

Polymerization

(2)

or, $j = \frac{\beta F^2}{5} \cdot \frac{1}{e^{\beta F l} - 1 - \beta F l}$ $\frac{1}{5} = \frac{D}{k_B T}$ $\frac{\beta F^2}{5} = \frac{1}{(k_B T)^2} F^2 D$

$$j = \frac{D F^2}{(k_B T)^2} \cdot \frac{1}{e^{\beta F l} - 1 - \beta F l}$$

as a check, as $F \rightarrow 0$ $e^{\beta F l} - 1 - \beta F l \approx 1 + \beta F l + \frac{1}{2}(\beta F l)^2 - 1 - \beta F l + \dots$
 $\approx \frac{1}{2} \beta^2 F^2 l^2 + \dots$

and $j \rightarrow \frac{D F^2}{(k_B T)^2} \cdot \frac{1}{\frac{1}{2} \beta^2 F^2 l^2} \approx \frac{2D}{l^2}$ as before ✓

when $\beta F l \gg 1$ $j \approx \frac{D F^2 e^{-\beta F l}}{(k_B T)^2}$

$$\tau = \frac{(k_B T)^2}{F^2 D} e^{\beta F l}$$

note $k_B T / F$ is a length, call it " δ "

$$\tau \approx \underbrace{\frac{\delta^2}{D}}_{\text{time to diffuse a distance } \delta} e^{\underbrace{\beta F l}_{\text{Boltzmann factor associated with work done on assembling polymer}}}$$

Wormlike chain

$$\mathcal{E} = \frac{1}{2} A \int_0^L ds \dot{x}^2 - f z$$

(1)

$$z = \int_0^L ds \cos(\theta(s)) \approx \int_0^L ds \left\{ 1 - \frac{1}{2} \theta^2(s) + \dots \right\} \approx L - \frac{1}{2} \int_0^L ds t_{\perp}^2$$

$$|t_{\perp}| \sim \theta \Rightarrow \mathcal{E} \approx \frac{1}{2} \int_0^L ds \left\{ A \left(\frac{\partial t_{\perp}}{\partial s} \right)^2 + f t_{\perp}^2 \right\} + \text{const}$$

$$\text{define } t_{\perp}(s) = \sum_g e^{-igs} \hat{t}_{\perp g}$$

$$\text{then } \mathcal{E} = \frac{1}{2} \int_0^L ds \left\{ \sum_g \sum_{g'} e^{-i(g+g')s} [-gg'A + f] \hat{t}_{\perp g} \hat{t}_{\perp g'} \right\} \quad \int_0^L ds e^{-i(g+g')s} = L \delta_{g, -g'}$$

$$= \frac{1}{2} \sum_g L (Ag^2 + f) |\hat{t}_{\perp g}|^2 \Rightarrow \langle |\hat{t}_{\perp g}|^2 \rangle = \frac{k_B T}{L(Ag^2 + f)}$$

x or y component

$$\text{length change} = \frac{1}{2} \int_0^L ds t_{\perp}^2 = \frac{1}{2} \sum_g \cdot \frac{2L k_B T}{L(Ag^2 + f)} \rightarrow \int_{-\infty}^{\infty} \frac{dg}{2\pi} \frac{L k_B T}{Ag^2 + f}$$

$$= \frac{L k_B T}{2\pi} \cdot \frac{1}{A} \int_{-\infty}^{\infty} \frac{dg}{g^2 + f/A}$$

$$\downarrow$$

$$L - z \approx \frac{L k_B T}{2} \cdot \frac{1}{\sqrt{fA}} \quad \text{or} \quad \boxed{1 - \frac{z}{L} \approx \frac{k_B T}{\sqrt{4fA}}}$$

$$\boxed{\frac{z}{L} \approx 1 - \frac{k_B T}{\sqrt{4fA}}}$$

rewriting this,

$$A = k_B T L_p$$

$$\left\{ f = \frac{k_B T}{L_p} \frac{1}{4(1 - z/L)^2} \right\}$$

Freely-jointed chain

WLC

(2)

$\langle b \rangle$

partition function of one link $Z_1 = \int_0^\pi d\theta \sin\theta e^{\beta f b \cos\theta}$

$$= \frac{2 \sinh(\beta f b)}{\beta f b}$$

$$\langle \text{displacement} \rangle = \frac{\partial \ln Z_1}{\partial \beta f} = b \left\{ \coth(\beta f b) - \frac{1}{\beta f b} \right\}$$

full $\langle \text{length} \rangle = N b \left\{ \coth(\beta f b) - \frac{1}{\beta f b} \right\}$ extended length = $N b$

$$\frac{\Delta \text{length}}{N b} = 1 - \frac{Z}{L} = 1 - \coth(\beta f b) + \frac{1}{\beta f b} \approx \frac{k_B T}{f b}$$

$\beta f b \gg 1$

$$\Rightarrow 1 - \frac{Z}{L} \approx \frac{k_B T}{f b} \quad \text{or} \quad \boxed{f \approx \frac{k_B T}{b} \frac{1}{(1 - Z/L)}}$$

Correlation function of WLC

$$= \frac{1}{L} \int_0^L dr \left\langle \sum_{\mathbf{q}} e^{-i \mathbf{q} \cdot \mathbf{r}} \hat{\mathbf{t}}_{\perp}(\mathbf{q}) \sum_{\mathbf{q}'} e^{-i \mathbf{q}' \cdot (\mathbf{r} + \mathbf{s})} \hat{\mathbf{t}}_{\perp}(\mathbf{q}') \right\rangle$$

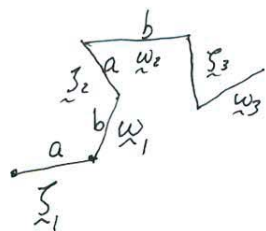
$$= \sum_{\mathbf{q}} e^{i \mathbf{q} \cdot \mathbf{s}} \langle |\hat{\mathbf{t}}_{\perp}(\mathbf{q})|^2 \rangle = \sum_{\mathbf{q}} \frac{k_B T}{L(A q^2 + f)} e^{i \mathbf{q} \cdot \mathbf{s}}$$

$$= \frac{2 k_B T}{A} \int \frac{d\mathbf{q}}{2\pi} \frac{e^{i \mathbf{q} \cdot \mathbf{s}}}{q^2 + f/A} = \frac{k_B T}{\sqrt{f A}} e^{-s \sqrt{f/A}} \quad \boxed{\sim e^{-s/\xi}} \quad \xi = \sqrt{A/f}$$

by contour integration

Polymer chains

a) ab polymer



let $\vec{\zeta}_n$ be bond vector for a type
 $\vec{\omega}_n$ ———— b

(1)

$$\vec{R} = \vec{r}_N - \vec{r}_0 = \sum_{m=1}^N \vec{\zeta}_m + \sum_{n=1}^N \vec{\omega}_n \quad \text{with } |\vec{\zeta}_n| = a \quad |\vec{\omega}_n| = b$$

$$|\vec{R}|^2 = \sum_{m=1}^N \vec{\zeta}_m \cdot \sum_{n=1}^N \vec{\zeta}_n + 2 \sum_{m=1}^N \vec{\zeta}_m \cdot \sum_{n=1}^N \vec{\omega}_n + \sum_{m=1}^N \vec{\omega}_m \cdot \sum_{n=1}^N \vec{\omega}_n$$

taking the average over realisations, we see that all x-terms such as $\langle \vec{\zeta}_l \cdot \vec{\omega}_n \rangle \rightarrow 0$
 and all off-diagonal self terms like $\langle \vec{\zeta}_l \cdot \vec{\zeta}_m \rangle \rightarrow 0$ for $l \neq m$, leaving only the diagonal terms:

$$|\vec{R}|^2 = \sum_{m=1}^N \vec{\zeta}_m^2 + \sum_{n=1}^N \vec{\omega}_n^2 = N \cdot a^2 + N \cdot b^2 = \boxed{N(a^2 + b^2)}$$

effective, average length² of compound segment.

stretching

$$\text{total } x = \sum l_n \cos \theta_n = \sum l_n^{(a)} \cos \theta_n^{(a)} + \sum l_n^{(b)} \cos \theta_n^{(b)}$$

$$\langle \bar{X} \rangle = \boxed{Na \langle \cos \theta^{(a)} \rangle + Nb \langle \cos \theta^{(b)} \rangle}$$

and Energy $E = -f\bar{X}$

$$\langle \cos \theta_l^{(a)} \rangle = \frac{\int d^2 \Omega_1 \dots \int d^2 \Omega_N \cos \theta_l^{(a)} e^{-\beta E}}{\int d^2 \Omega_1 \dots \int d^2 \Omega_N e^{-\beta E}}$$

any particular one

reduces to that of a single segment, since E is a linear combination

$$= \frac{\partial \ln Z_1^{(a)}}{\partial \beta f l^{(a)}} = \frac{\partial \ln Z_1^{(a)}}{\partial \beta f a} = \frac{\partial}{\partial \beta f a} \left\{ \text{const.} \frac{\sinh \beta f a}{\beta f a} \right\} = \boxed{\coth \beta f a - \frac{1}{\beta f a}}$$

thus,

$$\langle \bar{X} \rangle = Na \left\{ \coth \beta f a - \frac{1}{\beta f a} \right\} + Nb \left\{ \coth \beta f b - \frac{1}{\beta f b} \right\}$$

for small argument, $\coth(x) \approx \frac{1}{x} + \frac{1}{3}x + O(x^3)$

polymer chains

(2)

$$\langle \bar{X} \rangle \approx N a \cdot \frac{1}{3} \beta f a + N b \cdot \frac{1}{3} \beta f b \approx \frac{1}{3} \beta N (a^2 + b^2) f$$

$$\Rightarrow \boxed{f \approx \frac{3k_B T}{N(a^2 + b^2)} \langle \bar{X} \rangle}$$

$\underbrace{\hspace{1.5cm}}$
 k , effective spring constant.

b) FJC, a monomers only, restricted $0 \rightarrow \frac{\pi}{2}$ only

$$\langle \vec{r}_m \cdot \vec{r}_{m+1} \rangle = \langle \cos \theta \rangle = \frac{\int_0^{2\pi} \int_0^{\pi/2} d\phi \, d\theta \sin \theta \cos \theta}{\int_0^{2\pi} \int_0^{\pi/2} d\phi \, d\theta \sin \theta}$$

$$d\theta \sin \theta = -d \cos \theta$$

$$= \frac{\int_0^1 d(\cos \theta) \cos \theta}{\int_0^1 d(\cos \theta)} = \frac{\frac{1}{2} x^2 \Big|_0^1}{x \Big|_0^1} = \frac{1}{2}$$

Stretching in electric field

⑦

Simple: using previous solution of FJC in external field generating a force F ,

$$\frac{\langle x \rangle}{L} = \mathcal{L}(\beta F b) \quad \mathcal{L}(x) = \coth(x) - \frac{1}{x} \quad \text{is Langevin function}$$

$$L = Nb \text{ and } R_0 = \sqrt{N}b \text{ is radius of gyration}$$

$$\boxed{\frac{\langle x \rangle}{R_0} = \sqrt{N} \mathcal{L}(f)}$$

in this case, $F = qE = \begin{cases} \text{SI units} & 2 \cdot 10^3 \cdot 1.6 \times 10^{-19} \cdot 3 \times 10^3 \cdot 10^2 = 9.6 \times 10^{-11} \text{ N} = 96 \text{ pN} \\ \text{cgs} & 2 \cdot 10^3 \cdot 4.8 \times 10^{-10} \cdot 3 \times 10^3 \cdot \frac{1}{300} = 9.6 \times 10^{-6} \text{ dyne} \end{cases}$

$\frac{\text{V/cm}}{\downarrow} \quad \frac{\text{cm/m}}{\downarrow}$
 $\frac{\text{Volts}}{\text{statVolts}} \rightarrow 1 \text{ dyne} = 10^{-5} \text{ N} \quad \checkmark$

$$\beta F b = \frac{96 \text{ pN} \cdot 0.5 \text{ nm}}{4 \text{ pN nm}} \approx 12 \quad \mathcal{L}(12) \approx 0.92, \text{ almost fully extended}$$

to obtain 50% extension we need $\mathcal{L}(\beta F_{50} b) = 1/2$

using Matlab: $\text{fun} = @(x) \coth(x) - 1/x - 1/2;$

$$z = \text{fzero}(\text{fun}, 0.9)$$

$\uparrow$
guess

$$\Rightarrow \underline{\underline{z = 1.7968}}$$

$$\beta F_{50} b \approx 1.8$$

$$\frac{F_{50} \cdot 0.5 \text{ nm}}{4 \text{ pN nm}} = 1.8 \Rightarrow \underline{\underline{F_{50} \approx 14.4 \text{ pN}}}$$

A forced colloidal particle

1

$$\zeta \dot{x} = F(x - v_T t) \quad \text{let } y = x - v_T t \quad \left. \begin{array}{l} \dot{x} = \dot{y} + v_T \\ \dot{y} = \dot{x} - v_T \end{array} \right\}$$

$$\frac{dy}{dt} = \frac{F}{\zeta} - v_T \Rightarrow \int_{x_R}^{-x_L} \frac{dy}{F/\zeta - v_T} = \int dt = \Delta t \quad \text{assume } v_T > \max \left\{ \frac{F(y)}{\zeta} \right\}$$

in order of encounter

$$\Delta x = \Delta y + v_T \Delta t = \int_{x_R}^{-x_L} dy \left\{ 1 + \frac{v_T}{F/\zeta - v_T} \right\} = \int_{-x_L}^{x_R} dy \frac{F(y)}{\zeta v_T - F(y)}$$

$$\Rightarrow \Delta x = \int_{-x_L}^{x_R} dy \frac{F(y)}{\zeta v_T - F(y)}$$

note, $\frac{F(y)}{\zeta v_T - F(y)} > \frac{F(y)}{\zeta v_T}$

$$\downarrow > \int_{-x_L}^{x_R} dy \frac{F(y)}{\zeta v_T} = \frac{1}{\zeta v_T} \int dy F(y) = 0 \quad \text{since } F(y) = -\partial U / \partial y$$

$U = \text{trapping potential}$

$\therefore \Delta x > 0$

particle experiences backwards force for a shorter time than forwards force, as long as $v_T - F/\zeta > 0$ at is finite

$$\Delta t = \int_{-x_L}^{x_R} \frac{dy}{v_T - F(y)/\zeta}$$

could worry about special case

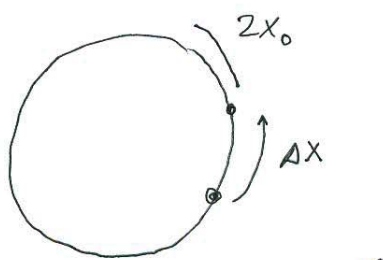
$$v_T - F(y)/\zeta \sim y^\alpha \quad \text{w/constant on } \alpha$$

for large v_T

$$\Delta x = \int \frac{dy F}{\zeta v_T (1 - F/\zeta v_T)} \approx \int dy \frac{(F + F^2/\zeta v_T + \dots)}{\zeta v_T}$$

$$\approx \int \frac{dy}{(\zeta v_T)^2} F^2(y) \quad \text{manifestly } > 0$$

circular orbit:



$$\Delta\theta = \frac{\Delta x}{R} : \text{after 1st kick, particle is caught again w/ extra time } \frac{2\pi R - 2x_0}{v_T}$$

$$= \frac{1}{f_T} \left(1 - \frac{x_0}{\pi R}\right)$$

$$f_T = \left(\frac{2\pi R}{v_T}\right)^{-1}$$

 $\therefore$ angular frequency is

$$\frac{\Delta x}{\Delta t + \frac{1}{f_T} \left(1 - \frac{x_0}{\pi R}\right)} \cdot \frac{1}{2\pi R}$$

for large trap velocity, $\Delta t \approx \frac{1}{v_T} \int dy = \frac{2x_0}{v_T} = \frac{1}{f_T} \cdot \frac{x_0}{\pi R}$

then $f_p = \frac{\Delta x}{2\pi R} \cdot \frac{1}{\frac{1}{f_T} \frac{x_0}{\pi R} + \frac{1}{f_T} \left(1 - \frac{x_0}{\pi R}\right)} \approx \frac{\Delta x}{2\pi R} f_T$

Triangular potential

$$\Delta x = \int_{x_0}^0 dy \frac{F}{3v_T - F} + \int_0^0 dy \frac{(-F)}{3v_T + F} = \frac{2x_0 v_c^2}{v_T^2 - v_c^2}$$

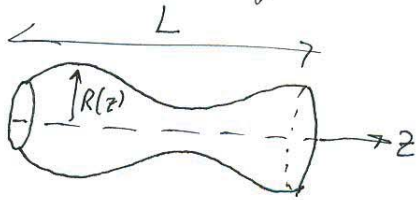
$$\Delta t = \frac{2x_0 v_T}{v_T^2 - v_c^2}$$

then (some algebra)

$$\left[\frac{f_p}{f_c} = \left(\frac{x_0}{\pi R}\right) \frac{f_T/f_c}{(f_T/f_c)^2 - 1} \left\{ 1 + \frac{(x_0/\pi R)}{(f_T/f_c)^2 - 1} \right\}^{-1} \right]$$

Fluctuations of circular objects

1



$$\text{Volume } V = \int dz \pi R^2(z)$$

$$\text{Surface area } S = \int dz 2\pi R \sqrt{1 + R_z^2}$$

write $R = \rho_0 + u_g \sin g z$ and adjust ρ_0 to conserve volume up to $O(u_g^2)$
(for consistency with application of equipartition theorem).

$$R^2 = \rho_0^2 + 2\rho_0 u_g \sin g z + u_g^2 \sin^2 g z$$

$$V = \underbrace{\pi \rho_0^2 L}_{\text{initially}} = \pi \rho_0^2 L + \underbrace{0}_{\int \sin g z = 0} + \pi u_g^2 \cdot \frac{1}{2} L = \pi L (\rho_0^2 + \frac{1}{2} u_g^2)$$

$$\therefore \rho_0 = R_0 \left[1 - \frac{u_g^2}{2R_0^2} \right]^{1/2} \approx R_0 \left(1 - \frac{1}{4} \frac{u_g^2}{R_0^2} + \dots \right)$$

$$\therefore \boxed{\rho_0 \approx R_0 - \frac{1}{4} \frac{u_g^2}{R_0} + \dots}$$

$$\text{look at surface area: } R \sqrt{1 + R_z^2} = (\rho_0 + \zeta) \left(1 + \frac{1}{2} \zeta_z^2 + \dots \right) \text{ where } \zeta = u_g \sin g z$$

$$= \rho_0 + u_g \sin g z + \frac{1}{2} \rho_0 g^2 u_g^2 \cos^2 g z + \dots$$

$$\therefore S = 2\pi \rho_0 L + 2\pi \cdot \frac{1}{2} \rho_0 g^2 u_g^2 \cdot \frac{1}{2} L = 2\pi L \rho_0 \left(1 + \frac{1}{4} g^2 u_g^2 + \dots \right)$$

$$= 2\pi L R_0 \left(1 - \frac{1}{4} \frac{u_g^2}{R_0^2} + \dots \right) \left(1 + \frac{1}{4} g^2 u_g^2 + \dots \right)$$

hence, the energy is

$$\sigma S = 2\pi L R_0 \sigma \left\{ 1 + \frac{1}{4 R_0^2} (g^2 R_0^2 - 1) u_g^2 + \dots \right\}$$

$$= \text{const} + \underbrace{\frac{\pi L}{2 R_0} \sigma [(g R_0)^2 - 1] u_g^2}_{\approx \frac{1}{2} k_B T \text{ when averaged}} + \dots$$

equipartition $\Rightarrow$

$$\boxed{\langle u_g^2 \rangle = \frac{k_B T R_0}{\pi L \sigma [(g R_0)^2 - 1]}}$$

clearly, for $g R_0 < 1$ there is a problem - the Rayleigh instability!

circular domain

Fluctuations of circular objects

(2)

write $\mathbf{r}(\theta) = (\rho_0 + \zeta) \hat{\mathbf{e}}_r$ $\hat{\mathbf{r}}_0 = \rho_0 \hat{\mathbf{e}}_r + (\rho_0 + \zeta) \hat{\mathbf{e}}_\theta$

area $A = \int d\theta \frac{1}{2} \mathbf{r} \times \hat{\mathbf{r}}_0 = \int d\theta \frac{1}{2} (\rho_0 + \zeta)^2$

initial area = $\pi R_0^2 = \pi \rho_0^2 + 0 + \frac{1}{2} \int d\theta u_g^2 \sin^2 \theta$
 $= \pi \rho_0^2 + \frac{1}{2} u_g^2 \cdot \frac{1}{2} \cdot 2\pi = \pi \rho_0^2 + \frac{\pi}{2} u_g^2$

$\Rightarrow \underline{\rho_0 = R_0 \left(1 - \frac{u_g^2}{2 R_0^2}\right)^{1/2}}$ as above

length of fluctuating domain:

$L = \int d\theta \sqrt{g} = \int d\theta \left[(\rho_0 + \zeta)^2 + \zeta_\theta^2 \right]^{1/2} = \rho_0 \left[\left(1 + \frac{\zeta}{\rho_0}\right)^2 + \frac{\zeta_\theta^2}{\rho_0^2} \right]^{1/2}$

$g = \hat{\mathbf{r}}_0 \cdot \hat{\mathbf{r}}_0$

$\left[1 + \frac{2\zeta}{\rho_0} + \frac{\zeta^2}{\rho_0^2} + \frac{\zeta_\theta^2}{\rho_0^2} \right]^{1/2} \approx 1 + \frac{\zeta}{\rho_0} + \frac{1}{2} \left(\frac{\zeta^2}{\rho_0^2} + \frac{\zeta_\theta^2}{\rho_0^2} \right)$

so, $L = \int d\theta \rho_0 \left\{ 1 + \frac{\zeta}{\rho_0} + \frac{1}{2} \frac{\zeta_\theta^2}{\rho_0^2} + \dots \right\} \approx 2\pi \rho_0 + 0$

$+ \frac{1}{2} \cdot 2\pi \cdot \frac{1}{2} \cdot \rho_0^2 u_g^2$

$-\frac{1}{8} \cdot \frac{4\zeta^2}{\rho_0^2} + \dots$

energy:

$\gamma L = 2\pi \rho_0 \gamma + \frac{\gamma}{2\rho_0} \pi \rho_0^2 u_g^2 = 2\pi \gamma R_0 \left(1 - \frac{1}{4} \frac{u_g^2}{R_0^2} + \dots\right) + \frac{\pi}{2} \gamma \frac{\rho_0^2 u_g^2}{R_0}$ to leading order

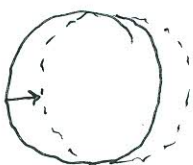
$= \boxed{2\pi \gamma R_0 + \frac{\pi \gamma}{2 R_0} \left((\gamma R_0)^2 - 1 \right) u_g^2}$

equipartition

$\frac{\pi \gamma}{2 R_0} [(\gamma R_0)^2 - 1] \langle u_g^2 \rangle = \frac{1}{2} k_B T$

$\boxed{\langle u_g^2 \rangle = \frac{k_B T R_0}{\pi \gamma [(\gamma R_0)^2 - 1]}}$

note: $\gamma R_0 = 1$ mode is a translation; no energy cost



Elastic filament fluctuations

(1)

a) $\mathcal{E} = \frac{1}{2} A \int_0^L dx h_{xx}^2$

Euler-Lagrange operator is ∂_{xx} , and for it to be self-adjoint

we need:

$$\int_0^L h_{xx} g dx = \int h g_{xx} dx$$

integrate by parts $\rightarrow h_{3x} g \Big|_0^L - \int_0^L h_{3x} g_x dx$
 $- h_{xx} g_x \Big|_0^L + \int_0^L h_{xx} g_{xx} dx$
 $h_x g_{xx} \Big|_0^L - \int_0^L h_x g_{3x} dx$
 $- h g_{3x} \Big|_0^L + \int_0^L h g_{4x} dx$

surface terms are

$$\left[h_{3x} g \Big|_0^L - h_{xx} g_x \Big|_0^L + h_x g_{xx} \Big|_0^L - h g_{3x} \Big|_0^L \right]$$

self-adjointness requires these to vanish, and if b.c.s are symmetric (same at both ends), we need only consider, say, the 1st 2 terms. In each case, we choose 1 out of 2 factors in $h_{3x} g$ and 1 out of 2 in $h_{xx} g_x \Rightarrow$ 4 possibilities

$h_{3x} = 0$ $h_{xx} = 0$

$h = 0$ $h_{xx} = 0$

h = position

$h_{3x} = 0$ $h_x = 0$

$h = 0$ $h_x = 0$

h_x = slope (if 0, "clamped")

h_{xx} = curvature
($A h_{xx}$ is a torque)

h_{3x} = curvature density

($A h_{3x}$ is a force)

clamped: $h = h_x = 0$ @ $x=0, L$

hinged: $h = h_{xx} = 0$ @ $x=0, L$ no torque

torqued: $h_x = h_{3x} = 0$ @ $x=0, L$ no force

free: $h_{xx} = h_{3x} = 0$ @ $x=0, L$ force free, torque free

b) for C-C conditions $W(x) = A \cosh kx + B \sinh kx + D \cosh kx + E \sinh kx$

$W(0) = \boxed{0 = A + D}$

$W(L) = \boxed{A \cosh kL + B \sinh kL + D \cosh kL + E \sinh kL = 0}$

$W_x = k [-A \sinh kx + B \cosh kx + D \sinh kx + E \cosh kx]$

$$\therefore W_x(0) = \boxed{k(B+E) = 0} \quad \boxed{W_x(L) = k[-A \sinh kL + B \cosh kL + D \sinh kL + E \cosh kL] = 0}$$

4 eqns for 4 unknowns (A, B, D, E)

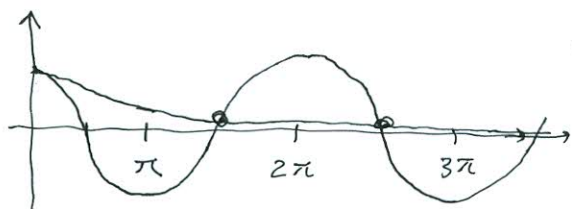
$\Rightarrow D = -A, E = -B$ and the remaining 2 eqns reduce to:

$$A \{ \cosh kL - \cosh kL \} + B \{ \sinh kL - \sinh kL \} \Rightarrow B = \frac{\cosh kL - \cosh kL}{\sinh kL - \sinh kL} A$$

$$\text{and } A \{ \sinh kL + \sinh kL \} = B \{ \cosh kL - \cosh kL \} = \frac{[\cosh kL - \cosh kL]^2}{\sinh kL - \sinh kL} A$$

$$\Rightarrow (\cosh kL - \cosh kL)^2 = \sinh^2 kL - \sinh^2 kL$$

$$\text{or } \boxed{\cosh kL \cosh kL = 1} \Rightarrow \boxed{\cosh kL = \frac{1}{\cosh kL}}$$



one root @ $k=0$

$$kL \gg 1 \quad (n + \frac{1}{2})\pi = (2n+1)\frac{\pi}{2} \quad n=1, 2, \dots$$

$$\begin{aligned} \text{c) } \mathcal{E} &= \frac{1}{2} A \int_0^L dx h_{xx}^2 = \frac{1}{2} A \left\{ h_x h_{xx} \Big|_0^L - \int_0^L dx h_x h_{3x} \right. \\ &\quad \left. - h h_{3x} \Big|_0^L + \int_0^L dx h h_{4x} \right\} = \frac{1}{2} A \int_0^L dx h h_{4x} \end{aligned}$$

$$\text{but if } h = \sum_n a_n W^{(n)}(x), \quad h_{4x} = \sum_n a_n W_{4x}^{(n)} \quad \text{and } W_{4x}^{(n)} = k^{(n)4} W^{(n)}$$

$$\Rightarrow \boxed{\mathcal{E} = \frac{1}{2} A \int_0^L dx \sum_m a_m W^{(m)} \sum_n a_n k^{(n)4} W^{(n)}}$$

if we assume the W s are orthonormal

$$\mathcal{E} = \frac{1}{2} A \sum_m k^{(m)4} a_m^2$$

so, by equipartition

$$\boxed{\langle a_m^2 \rangle = \frac{k_B T}{A k^{(m)4}}}$$

$$\text{and } \langle h^2(x) \rangle = \left\langle \sum_m \sum_n a_m a_n W^{(m)}(x) W^{(n)}(x) \right\rangle$$

$$= \sum_n \frac{k_B T}{A k^{(n)4}} W^{(n)}(x)^2$$

and $\langle a_m a_n \rangle = \delta_{m,n}$ since modes are independent and Gaussian

d) if $\mathcal{E} = \frac{1}{2} \int_0^L dx \left\{ A h_{xx}^2 + \sigma(x) h_x^2 \right\}$ $\sigma(0) = \sigma(L) = 0$

$\downarrow$ integrate by parts $\Rightarrow \sigma h_x h \Big|_0^L - \int_0^L dx (\sigma h_x)_x h$

hence, E-L eqn is $\boxed{A h_{4x} - [\sigma(x) h_x]_x = 0}$

if $A W_{4x}^{(n)} - [\sigma(x) W_x^{(n)}]_x = \lambda^{(n)} W^{(n)}$ (not solving explicitly)

$$\mathcal{E} = \frac{1}{2} \int dx \left\{ A h_{4x} - [\sigma(x) h_x]_x \right\} h \Rightarrow \frac{1}{2} \int_0^L dx \sum_m \lambda^{(m)} a_m w^{(n)}(x) \sum_n a_n w^{(n)}$$

$$\parallel$$

$$\frac{1}{2} \sum_m \lambda^{(m)} a_m^2$$

and equipartition can be applied in the usual way.