

# Viscoelastic flow through a contraction

Progress and Problems

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## Refereeing :

Boyko, E. & Stone, H. A. (2022) *Pressure-driven flow of the viscoelastic Oldroyd-B fluid in narrow non-uniform geometries: analytical results and comparison with simulations*. JFM 936

## Recall:

Hinch, E.J. (1993) *The flow of an Oldroyd fluid around a sharp corner*. JNNFM 40

Realise: A new application for an old FAST trick!

# Simplifications

1. Slowly varying = lubrication theory, with boost for tension in streamlines
2. Oldroyd-B

$$\boldsymbol{\sigma} = -p\mathbf{I} + 2\mu_0\mathbf{e} + G\mathbf{A}.$$

Microstructure  $\mathbf{A}$  deforms with the flow (upper-convective time derivative), and relaxes

$$\overset{\nabla}{\mathbf{A}} = \frac{D\mathbf{A}}{Dt} - \mathbf{A} \cdot \nabla \mathbf{u} - \nabla \mathbf{u}^T \cdot \mathbf{A} = -\frac{1}{\tau}(\mathbf{A} - \mathbf{I}).$$

# Fast flow trick

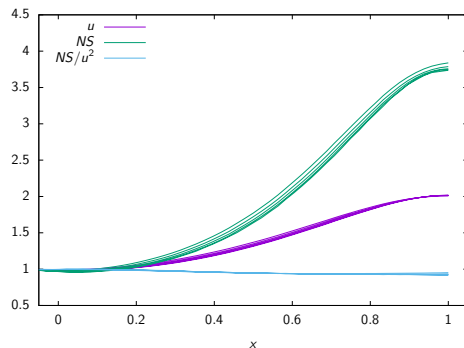
Fast = no time to relax

$$\nabla \mathbf{A} = \frac{D\mathbf{A}}{Dt} - \mathbf{A} \cdot \nabla \mathbf{u} - \nabla \mathbf{u}^T \cdot \mathbf{A} = -\frac{1}{\tau} (\mathbf{A} - \mathbf{I}).$$

Solution:  $\mathbf{A} = \lambda(\psi)\mathbf{u}\mathbf{u}$

Plot variation along streamlines  
through the contraction

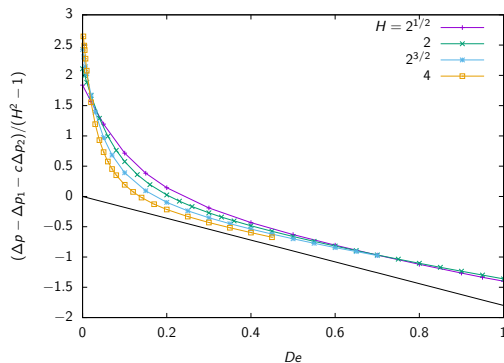
Conclude  $A \propto u^2$  on streamlines



## Fast flow 2

Hence predict stress and pressure drop for large  $De$  ( $> 0.3$ )

$$\Delta p = \Delta p_1 + c\Delta p_2 - \frac{9cDe}{5} (H^2 - 1).$$



Different planar contraction ratios,  $c = 1.0$ .

# Problem 1. Relaxation after the contraction

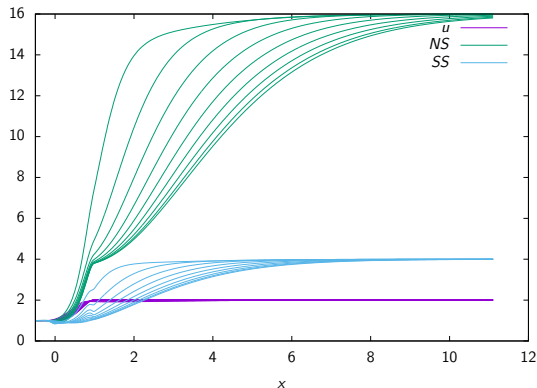
Too many recent papers have just found the pressure drop **in the contraction** .

Contraction in  $0 \leq x \leq 1$

Planar contraction

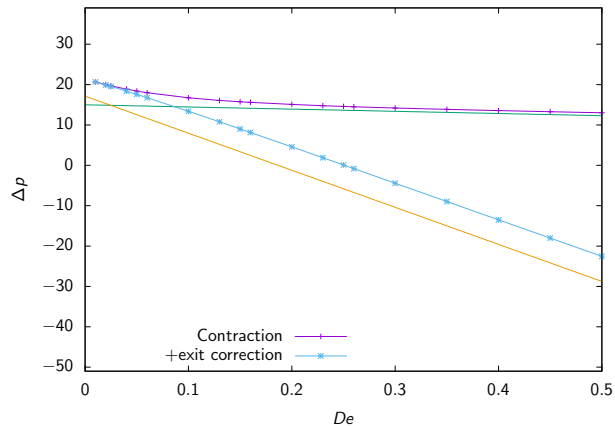
$De = 0.5$ ,  $H = 2$ ,  $c = 1.0$

Need to go to  $x = 8$   
for 95% relaxation



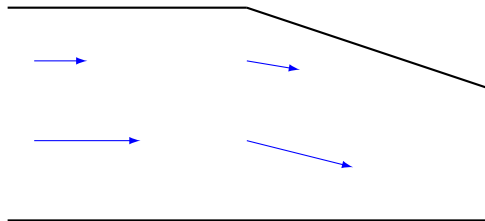
## exit channel correction

Planar contraction  $De = 0.5$ ,  $H = 2$ ,  $c = 1.0$



Neglected exit channel dominates change in pressure drop!

## Problem 2. Non-smooth boundary



Discontinuity of slope of boundary,  
→ discontinuity in  $y$ -velocity  
(in lubrication theory picture),  
→  $\delta$ -function of vorticity,  
→ jump in direction of elastic stresses

$$A_{xx}(0+) = A_{xx}(0-),$$

$$A_{xy}(0+) = A_{xy}(0-) + \eta A_{xx}(0-),$$

$$A_{yy}(0+) = A_{yy}(0-) + 2\eta A_{xy}(0-) + \eta^2 A_{xx}.$$

where  $\eta = yH'(0+)/H^2(0)$

Avoid with smooth boundary or streamline coordinates

### Problem 3. Naive small- $De$ expansion

$$\overset{\nabla}{\mathbf{A}} = \frac{D\mathbf{A}}{Dt} - \mathbf{A} \cdot \nabla \mathbf{u} - \nabla \mathbf{u}^T \cdot \mathbf{A} = -\frac{1}{De} (\mathbf{A} - \mathbf{I}).$$

Iterate

$$\mathbf{A} = \mathbf{I} - De \overset{\nabla}{\mathbf{I}} + De^2 \overset{\nabla \nabla}{\mathbf{I}} - De^3 \overset{\nabla \nabla \nabla}{\mathbf{I}} + De^4 \overset{\nabla \nabla \nabla \nabla}{\mathbf{I}} + \dots$$

with no opportunity to satisfy inlet stress boundary condition.

Several recent papers have made this naive expansion to many,  $O(De^8)$ , erroneous terms.

## For hyperbolic contraction

$$R(z) = \frac{1}{(1 + \beta z)^{1/2}}$$

with jump in shape (so fail to satisfy inlet condition)

$$A_{22} = 1 - De\beta F + De^2\beta^2 F^2 - De^3\beta^3 F^3 + \dots$$

Summing

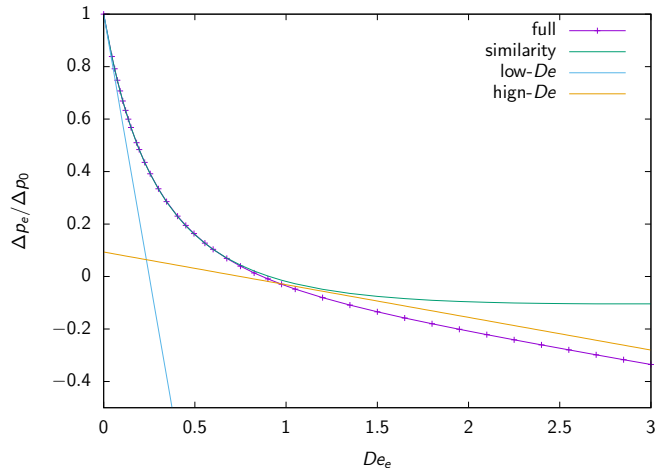
$$A_{22} = \frac{1}{1 + De\beta F}.$$

and similar for  $A_{12}$  and  $A_{11}$ .

This is the [exact/similarity solution](#) of Sialmas & Housiadas, NOT satisfy inlet stress condition.

Panagiotis Sialmas & Kostas D. Housiadas (2025) *An exact solution of the lubrication equations for the Oldroyd-B model in a hyperbolic pipe* JNNFM 335

## Problem 4: Similarity solutions fails badly at $De_e > 1$



Integrating pressure gradient

$$\int_0^1 \frac{dz}{(1 + \beta z)^{1/De-1}}$$

Dominated by  $x$  near 1  
to all  $O(De^n)$  for  $De < 0.5$

Then switch to whole range

# Conclusions

- ▶ Progress: Fast flow
- ▶ Problem: need long exit channel
- ▶ Problem: need smooth geometry
- ▶ Problem: small- $De$  expansion could be naive (wrong)
- ▶ Problem: a new similarity solutions fails badly at  $De_e > 1$